

THE FORMATION OF PYROCHLORES DURING PLASMA SPRAYING OF REO AND ZIRCONIA OXIDES POWDER MIXTURE

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Abstract: The pyrochlores are the promising low-thermal conductive materials for Thermal Barrier Coatings applications. In present work the concept of pyrochlore formation during APS spraying of ZrO₂ and ReO was analyzed. The specially prepared agglomerated mixtures of ZrO₂ with Nd₂O₃, Yb₂O₃, Er₂O₃ and Gd₂O₃ oxides were plasma sprayed using A60 plasma torch on NiCoCrAlY-type bond coat. The influence of plasma gasses composition on coatings' microstructure was investigated. The results of XRD phase analysis proved formation of pyrochlores from Gd₂O₃ +ZrO₂ and Nd₂O₃+ZrO₂ mixtures. The formation of Er₄O₁₂Zr₃ from Er₂O₃+ ZrO₂ mixture as well as Zr₃Yb₄ from Yb₂O₃+ ZrO₂ powder was detected. The presence of pure rare earth oxides (REO) and zirconia oxides was observed in all types of sprayed coatings. The microstructural assessment showed differences in porosity and thickness of obtained ceramic coatings depending of type of REO oxides. The analysis of results showed that it is possible to obtain pyrochlore ceramic coatings from pure oxides mixture. The plasma energy was not efficient for full formation of pyrochlores, therefore the presence of pure oxides was observed.

Keywords: Thermal Barrier Coatings, plasma spraying, ceramic coating, rare earth oxides, pyrochlores, porosity

1. INTRODUCTION

The increase of the turbine entry temperature of the turbine inlet temperature (TIT) determines the development of new materials used in construction of modern jet engines. The use of manufacturing process of turbine blades and vanes from nickel superalloys and modification of their chemical composition increased their heat stability [1]. At the same time, their resistance against high-temperature corrosion has decreased. Therefore, it is necessary to introduce heat-resistant layers and coatings, which protect the substrate of the nickel superalloy. Particularly effective way of protecting the surface of components of the hot air section of a turbine aircraft engine is the use of thermal barrier coatings (TBCs). TBCs are always composed of at least two layers - the outer ceramic layer - most often zirconium oxide stabilized with

ZrO₂*nY₂O₃ - YSZ (Yttria Stabilized Zirconia) - and an internal - MCrAlY type, metallic bond coat. Introduction of an outer ceramic layer enabled to effectively increase protection of the nickel superalloy substrate against the impact of the exhaust gas stream. In aerospace industry, thermal barrier coatings are produced primarily in the air plasma spray process (APS) [2]. Recently the development of thermal barrier coatings is oriented on using new ceramic materials characterized by lower thermal conductivity and higher working temperature [3]. The most promising materials are silicide, mulite and rare-earth oxides (REO) [4,5]. In recent time the research work is concerned on ceramic layers based on rare earth zirconates such as Gd₂Zr₂O₇ [6], Nd₂Zr₂O₇ [7], Sm₂Zr₂O₇ [8]. This type of coatings is thermally sprayed using specially prepared ceramic powders. Those powders are produced by calcination of rare-earth oxides with zirconia oxide and fractionation for using plasma-spraying process. [9-10]. In the present

work the concept of formation REO zirconates during plasma spraying of REO and ZrO₂ mixture was verified. The selection of those oxide components content in powder was oriented on formation of REO zirconates during thermal spray process.

2. MATERIALS AND METHODS

The stainless steel X2CrNiMo17-12-2-type was used as a base material for the TBC systems. A60 plasma torch (Thermico) was used for thermal spraying of bond coat as well as for ceramic layer of thermal barrier coating. The NiCoCrAlY bond coat was plasma sprayed using Amdry 386 powder (Oerlikon Metco) using process parameters presented in Table 1.

Tab. 1. The bond coat spraying parameters

Parameter	Value
Powder feed rate, g/min	10
Power current, A	550
Ar flow rate, dm ³ /min	70
Hydrogen flow rate, dm ³ /min	4

The ceramic powders were prepared by ball milling and agglomerating of pure ZrO₂ and REO oxides. Their chemical composition was selected for easy formation of pyrochlore-type phases during plasma spray process. The chemical composition of used powders is presented in Table 2.

Tab. 2 The chemical composition of powders used for plasma spraying

Mixture type	ZrO ₂ content (wt. %)	REO type	REO content (wt. %)
Gd ₂ O ₃ +ZrO ₂	40	Gd ₂ O ₃	60
Er ₂ O ₃ +ZrO ₂	39	Er ₂ O ₃	61
Nd ₂ O ₃ +ZrO ₂	42.3	Nd ₂ O ₃	57.7
Yb ₂ O ₃ +ZrO ₂	61.5	Yb ₂ O ₃	38.5

To investigate the effect of plasma enthalpy on structure of ceramic coating the different compositions of Ar/H₂ ratio were used (Table 3). The other process parameters were constant: power current: 700A, powder feed rate: 10 g/min, plasma torch movement speed: 50 mm/s.

Tab. 2. Ceramic layer spraying parameters

Plasma gasses flow rate, dm ³ /min		Ar/ H ₂ ratio
Ar	H ₂	
60	12	5:1
48	12	4:1
60	6	10:1

Powders and coatings morphologies were investigated using scanning electron microscopy (SEM) Hitachi S3400N equipped with energy dispersive spectroscopy (EDS) detector. The thickness and porosity of coatings were measured on digital images using Aphelion 3.1. software. The phase analysis was conducted by X-ray Diffraction (XRD)

using XTRa ARL diffractometer (Thermo Fisher). The obtained spectra were identified using ICDD database (International Centre For Diffraction Data).

3. RESULTS AND DISCUSSION

3.1. Morphology of obtained ceramic powders

The initial microscopic assessment showed that powders prepared by ball milling and mixing possess different morphology, which not permit them to be used for thermal spray process. The problems with powder feeding and blocking were previously observed. For thermal spraying technology special method of agglomeration of powders was developed, namely spray drying process with addition of special chemical additives was performed. The analysis of final powders morphology showed formation of agglomerated particles from equiaxed grains with size ranged from 100 nm to 2 μm (Fig. 2 a-d)

3.2. Roughness of coating

The lowest roughness after thermal spraying was measured on surface of coatings formed from powder mixtures Er₂O₃+ZrO₂ (R_a=6.66 μm) and Yb₂O₃+ZrO₂ (R_a=6 μm) (Fig 1). The highest roughness (over R_a=15 μm) on surface of Nd₂O₃+ZrO₂ plasma sprayed coating was measured. It was shown that this factor strongly depends of grain size as well as morphology of thermally sprayed powders.

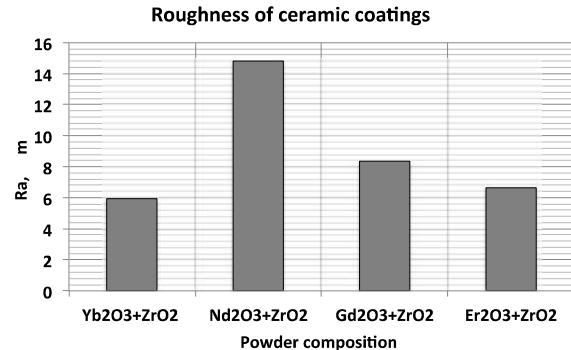


Fig. 1. Average roughness of plasma sprayed ceramic coating using different oxides mixture

3.3. Coatings sprayed using Yb₂O₃+ZrO₂ powders

The results of microscopic investigation showed that plasma gasses composition and flow rate strongly influence coating porosity and their thickness (Fig 3). It was shown that thickness of coatings sprayed using gas mixtures: H₂=6 dm³/min Ar=60 dm³/min as well as H₂=12 dm³/min and Ar=48 dm³/min did not exceed 40 μm (Fig. 3a). Thicker coating was formed when H₂=12 dm³/min and Ar=60 dm³ plasma gasses mixture was used. The increasing of hydrogen flow caused a reduction of coatings porosity from 35% to about 25%.

The results of XRD phase analysis of thermally sprayed coating revealed the presence of oxides used for thermal spraying Yb₂O₃ and ZrO₂ as well as Zr₃Yb₄ phase (Fig. 4). The REO pyrochlores were not detected.

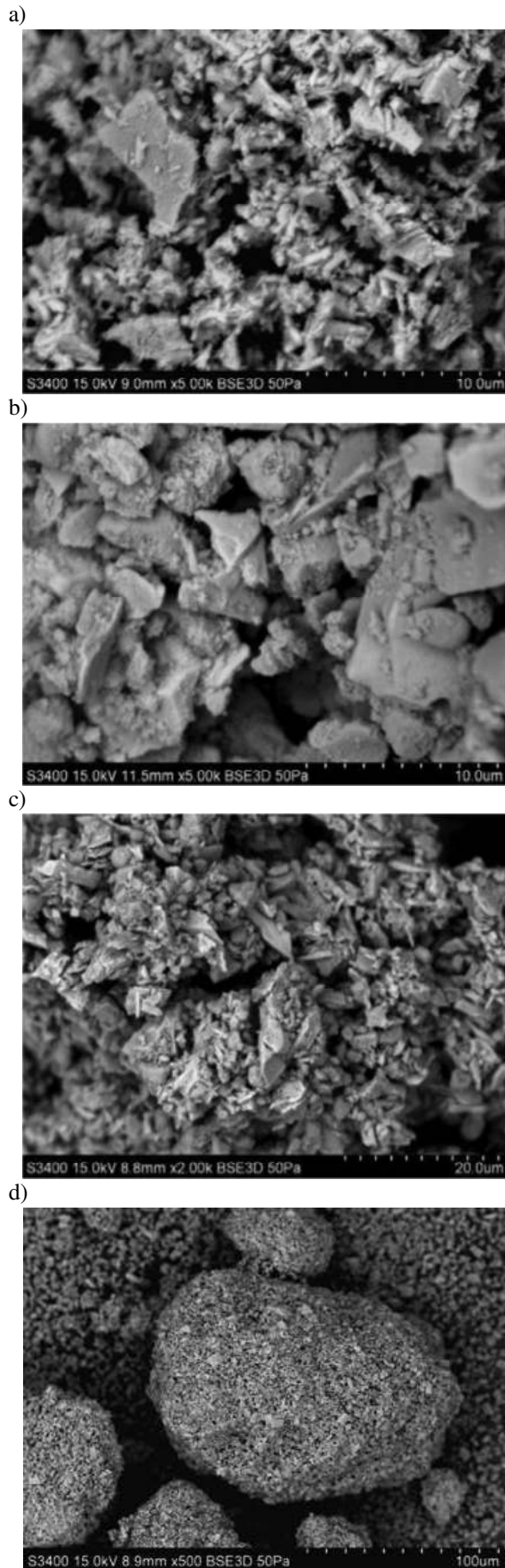


Fig. 2. Morphology of agglomerated powders used in experimental: a) $Gd_2O_3+ZrO_2$ b) $Er_2O_3+ZrO_2$, c) $Yb_2O_3+Zr_2O_3$, d) $Nd_2O_3+Zr_2O_3$

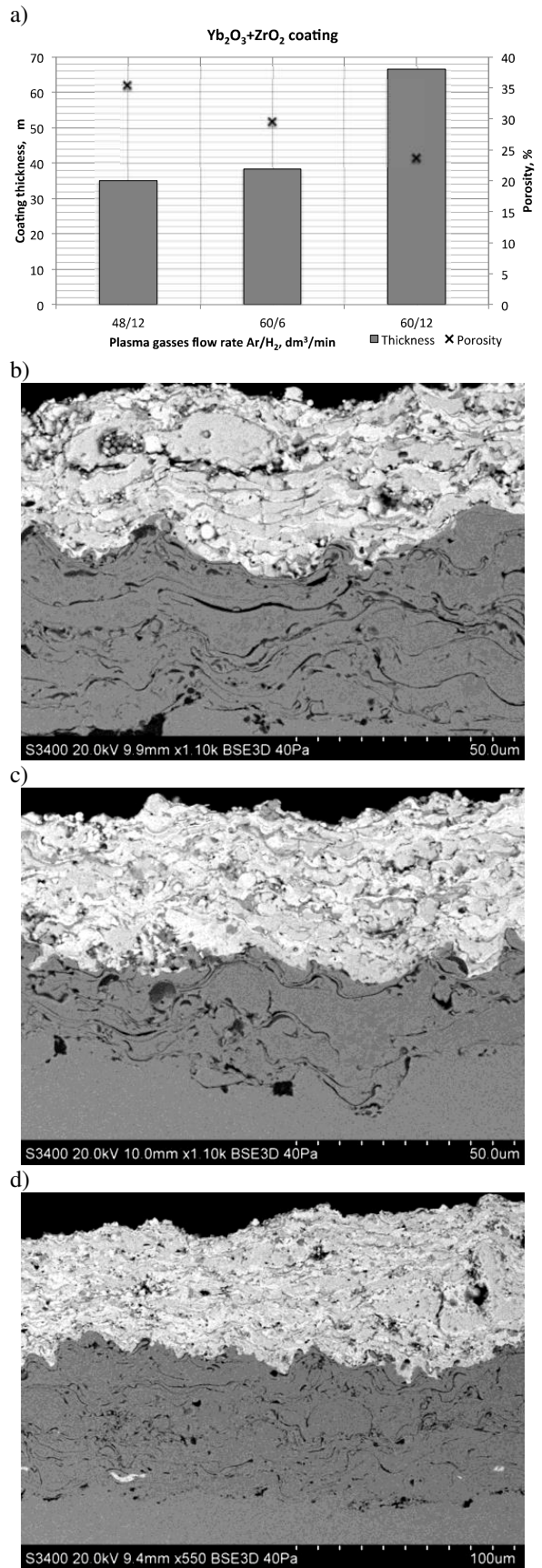


Fig. 3. The porosity and thickness (a) and microstructure of ceramic coatings formed by plasma spraying of Yb₂O₃+ZrO₂ powder with plasma gases flow: b) H₂=12 dm³/min + Ar=48 dm³/min c) H₂=12 dm³/min and Ar=60 dm³/min and d) H₂=12 dm³/min and Ar=60 dm³

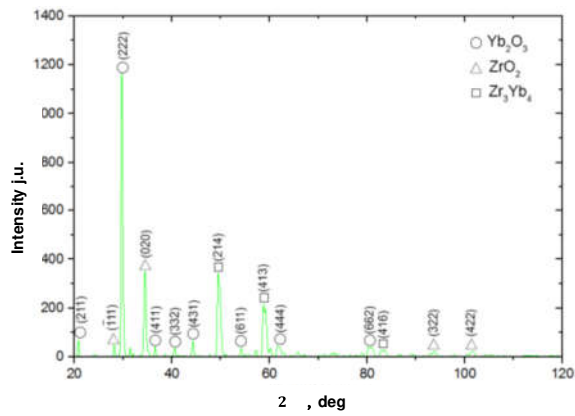


Fig. 4. XRD diffraction pattern from surface of ceramic layer plasma sprayed using $\text{Yb}_2\text{O}_3 + \text{ZrO}_2$ powders mixture and gas composition: $\text{H}_2=12 \text{ dm}^3/\text{min}$ and $\text{Ar}=60 \text{ dm}^3$

3.4. Coatings sprayed using $\text{Nd}_2\text{O}_3 + \text{ZrO}_2$ powder

The using of higher hydrogen flow rate ($\text{H}_2=12 \text{ dm}^3/\text{min}$) in plasma gasses mixture, independently of Ar flow enables to form thick coating ($80\text{-}95 \mu\text{m}$) with lower porosity (about 30%) (Fig. 5). If hydrogen flow rate was lower the obtained coating thickness was smaller than $70 \mu\text{m}$ and their porosity was higher ($>45\%$).

The XRD phase analysis (Fig. 6.) showed the presence of neodymium zirconate $\text{Nd}_2\text{Zr}_2\text{O}_7$ as well as $\text{Nd}_{1.85}\text{Zr}_{0.1}\text{O}_3$ phase. The zirconia oxide was also detected.

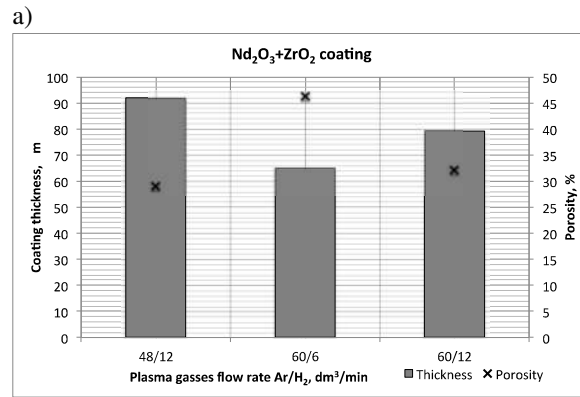
3.5. Coatings sprayed using $\text{Er}_2\text{O}_3 + \text{ZrO}_2$ powders

The ceramic coatings sprayed using $\text{Er}_2\text{O}_3 + \text{ZrO}_2$ powder and low plasma gasses flow ($\text{H}_2=12 \text{ dm}^3/\text{min}$ and $\text{Ar}=48 \text{ dm}^3/\text{min}$) was characterized by lower porosity (about 25%) and thickness (about $75 \mu\text{m}$) (Fig. 9). The increase of overall plasma flow enabled to increase the coating thickness above $110 \mu\text{m}$. As a consequence the higher coating porosity (in range 30-35 %) was measured.

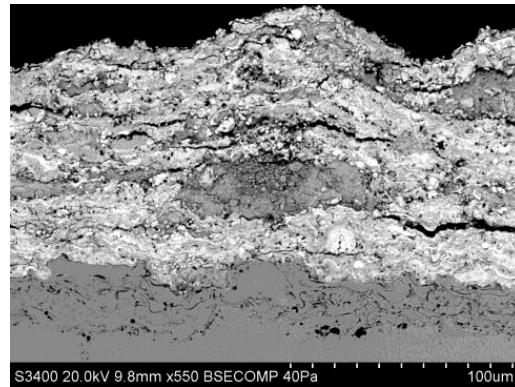
The phase composition analysis showed the presence of $\text{Er}_4\text{O}_{12}\text{Zr}_3$ phase as well as components from plasma sprayed powder, namely erbium and zirconium oxides (Fig. 7).

3.6. Coatings sprayed using $\text{Gd}_2\text{O}_3 + \text{ZrO}_2$ powders

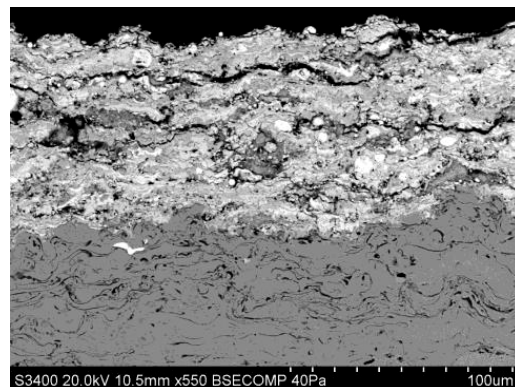
The using of higher overall plasma gasses flow ($\text{H}_2=12 \text{ dm}^3/\text{min}$ and $\text{Ar}=60 \text{ dm}^3$) enables to obtain the ceramic coating with the highest thickness ($>70 \mu\text{m}$) and the lowest porosity (25%) (Fig. 10). The decreasing of plasma gasses flow rate reduces the plasma enthalpy and as a result- decreases coatings thickness ($55\text{-}66 \mu\text{m}$) and increases their porosity ($>45\%$) The XRD phase analysis showed the presence of gadolinium zirconate ($\text{Gd}_2\text{Zr}_2\text{O}_7$) as well as components of plasma sprayed powder (ZrO_2 and Gd_2O_3) (Fig. 8).



b)



c)



d)

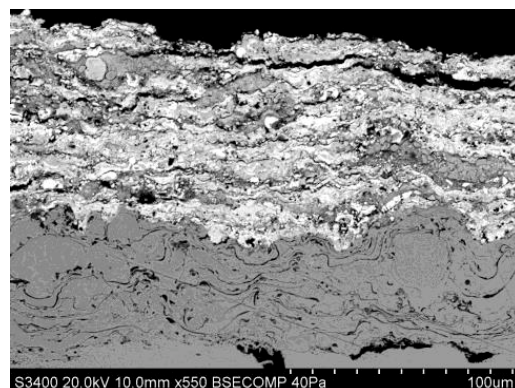


Fig. 5. The porosity and thickness (a) and microstructure of ceramic coatings formed by plasma spraying of $\text{Nd}_2\text{O}_3 + \text{ZrO}_2$ powder with plasma gasses flow: b) $\text{H}_2=12 \text{ dm}^3/\text{min} + \text{Ar}=48 \text{ dm}^3/\text{min}$ c) $\text{H}_2=12 \text{ dm}^3/\text{min}$ and $\text{Ar}=60 \text{ dm}^3/\text{min}$ and d) $\text{H}_2=12 \text{ dm}^3/\text{min}$ and $\text{Ar}=60 \text{ dm}^3$

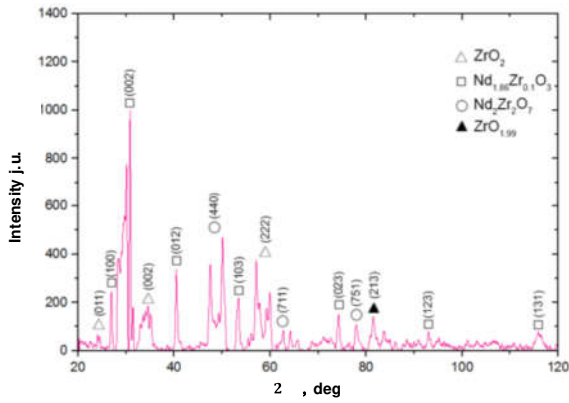


Fig. 6. XRD diffraction pattern from surface of ceramic layer plasma sprayed using $\text{Nd}_2\text{O}_3 + \text{ZrO}_2$ powders mixture and gas composition: $\text{H}_2 = 12 \text{ dm}^3/\text{min}$ and $\text{Ar} = 60 \text{ dm}^3$

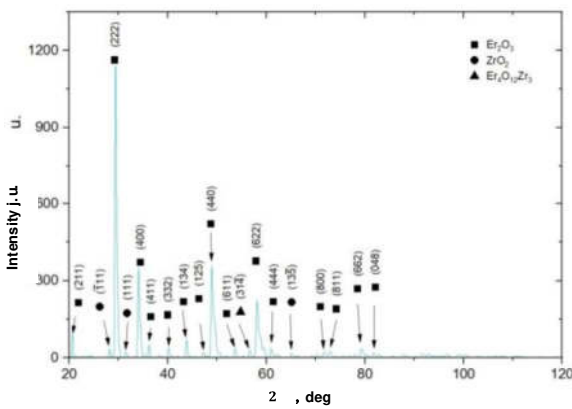


Fig. 7. XRD diffraction pattern from surface of ceramic layer plasma sprayed using $\text{Er}_2\text{O}_3 + \text{ZrO}_2$ powders mixture and gas composition: $\text{H}_2 = 12 \text{ dm}^3/\text{min}$ and $\text{Ar} = 60 \text{ dm}^3$

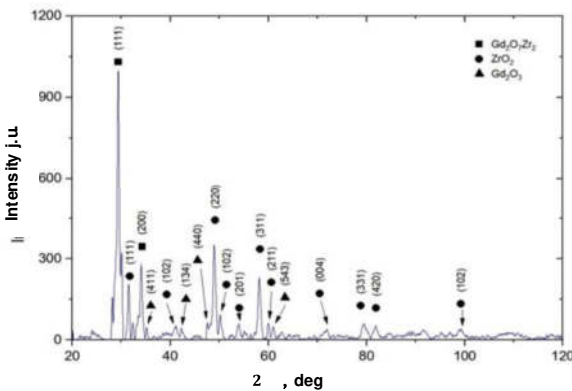


Fig. 8. XRD diffraction pattern from surface of ceramic layer plasma sprayed using $\text{Gd}_2\text{O}_3 + \text{ZrO}_2$ powders mixture and gas composition: $\text{H}_2 = 12 \text{ dm}^3/\text{min}$ and $\text{Ar} = 60 \text{ dm}^3$

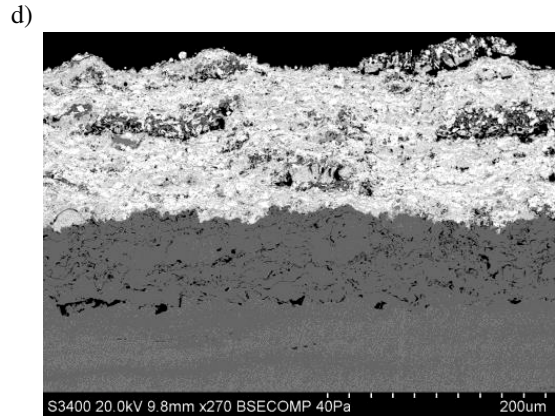
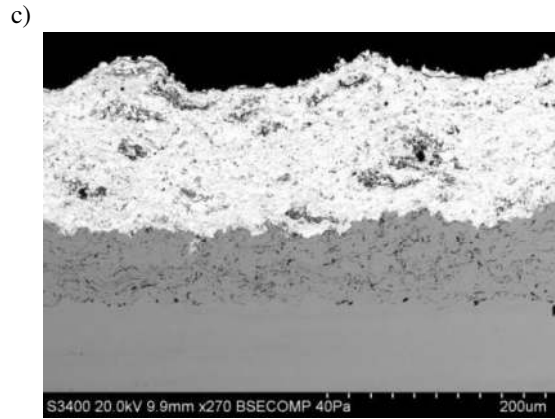
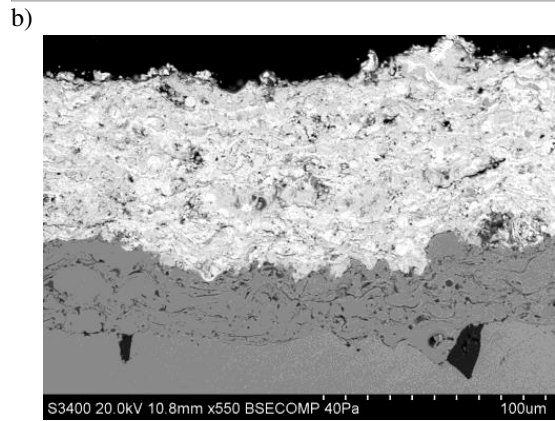
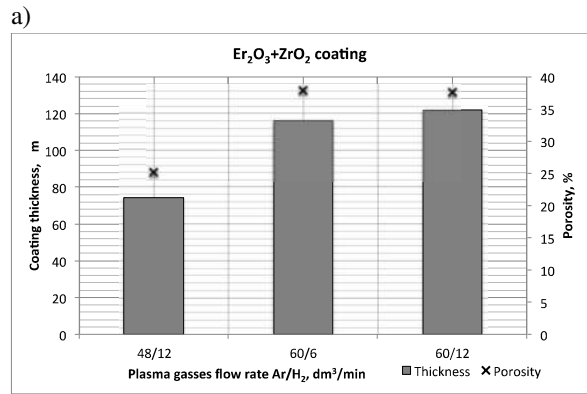


Fig. 9. The porosity and thickness (a) and microstructure of ceramic coatings formed by plasma spraying of $\text{Er}_2\text{O}_3 + \text{ZrO}_2$ powder with plasma gasses flow: b) $\text{H}_2 = 12 \text{ dm}^3/\text{min} + \text{Ar} = 48 \text{ dm}^3/\text{min}$ c) $\text{H}_2 = 12 \text{ dm}^3/\text{min}$ and $\text{Ar} = 60 \text{ dm}^3/\text{min}$ and d) $\text{H}_2 = 12 \text{ dm}^3/\text{min}$ and $\text{Ar} = 60 \text{ dm}^3$

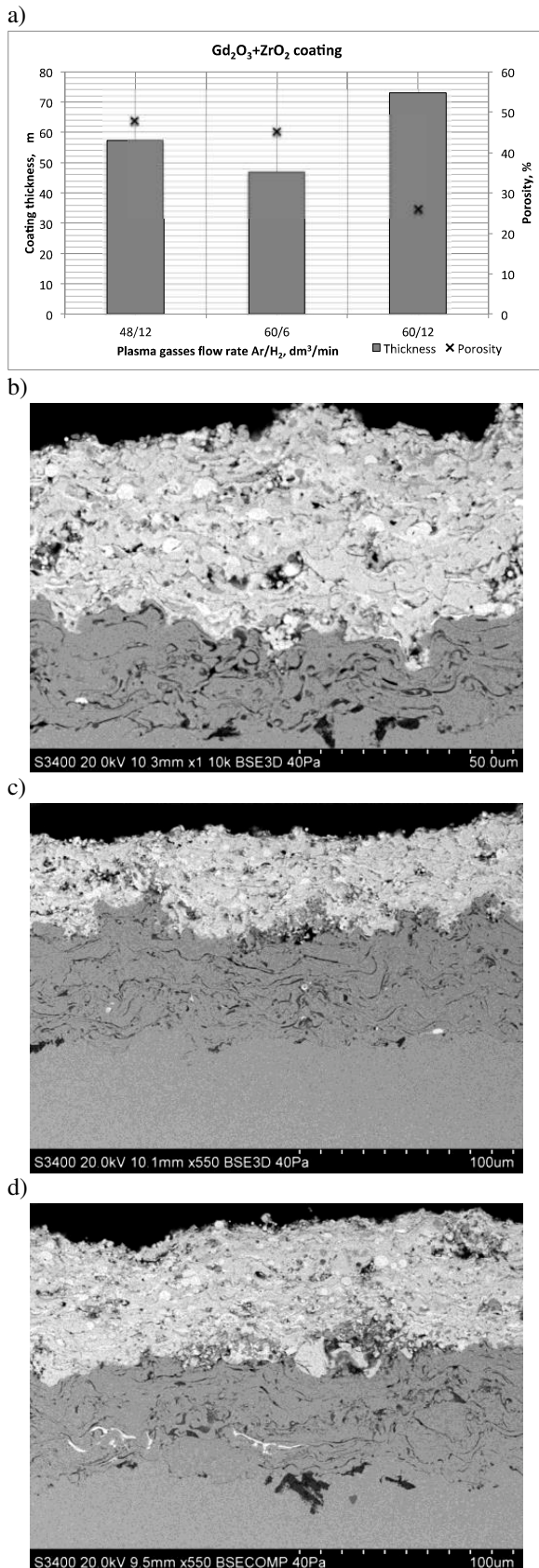


Fig. 10. The porosity and thickness (a) and microstructure of ceramic coatings formed by plasma spraying of Gd₂O₃+ZrO₂ powder with plasma gases flow: b) H₂=12 dm³/min + Ar=48 dm³/min c) H₂=12 dm³/min and Ar=60 dm³/min and d) H₂=12 dm³/min and Ar=60 dm³

4. CONCLUSIONS

The pyrochlores are the promising materials possessing low-thermal conductivity and can be used for Thermal Barrier Coatings application [6-10]. In conducted research concept of pyrochlore formation during APS spraying of ZrO₂ and REO was analysed. The specially prepared agglomerated mixture of ZrO₂ with Nd₂O₃, Yb₂O₃, Er₂O₃ and Gd₂O₃ oxides was plasma sprayed using A60 plasma torch on NiCoCrAlY-type bond coat. The influence of plasma gases composition on coatings' microstructure was investigated. It was shown that increasing of overall plasma gases flow as well as increasing of hydrogen flow rate leads to increase of plasma enthalpy. As a consequence of higher plasma energy, the thickness of ceramic coating was increased and the porosity was decreased.

The results of XRD phase analysis showed that plasma enthalpy had no influence of phase composition of obtained coatings. What is important, the pyrochlore Nd₂Zr₂O₇ was formed during thermal spraying of Nd₂O₃ and ZrO₂ oxides mixture. In this case the neodymium oxide formed pyrochlores and Nd_{1.86}Zr_{0.1}O₃ phase. The partial transformation of gadolinium and zirconium oxide into Gd₂Zr₂O₇ pyrochlore was observed. In the coating the pure oxides were present as well. During plasma spraying of ytterbium and zirconium oxide powders the Zr₃Yb₂ phase was formed. On the other hand the Er₄O₁₂Zr₃ phase was synthesized during thermal spraying of Er₂O₃ and ZrO₂ powders mixture.

The experimental results of thermal spraying processes showed that it is possible to obtain pyrochlore ceramic coatings from mixture of pure oxides. The plasma energy was not efficient to full formation of pyrochlores so the presence of pure oxides and formation of other phases was observed. In further test the other plasma torches characterized by higher plasma enthalpy enables to form pyrochlores during thermal spraying is planned to be done to avoid an additional calcination process prior plasma spraying process.

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